

Numerical Methods of Electromagnetic Field Theory II (NFT II) Numerische Methoden der Elektromagnetischen Feldtheorie II (NFT II) /

3rd Lecture / 3. Vorlesung

Dr.-Ing. René Marklein

marklein@uni-kassel.de

<http://www.tet.e-technik.uni-kassel.de>

<http://www.uni-kassel.de/fb16/tet/marklein/index.html>

Universität Kassel
Fachbereich Elektrotechnik / Informatik
(FB 16)
Fachgebiet Theoretische Elektrotechnik
(FG TET)
Wilhelmshöher Allee 71
Büro: Raum 2113 / 2115
D-34121 Kassel

University of Kassel
Dept. Electrical Engineering / Computer Science
(FB 16)
Electromagnetic Field Theory
(FG TET)
Wilhelmshöher Allee 71
Office: Room 2113 / 2115
D-34121 Kassel

2-D Versions of EFIE and MFIE: TM and TE Case / 2D-Versionen von EFIE und MFIE: TM- und TE-Fall

2-D Case /
2D-Fall

Position Vector / Ortsvektor

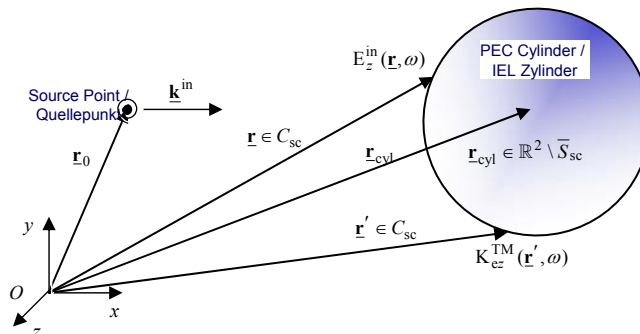
$$\underline{\mathbf{R}} = x\mathbf{e}_x + y\mathbf{e}_y + z\mathbf{e}_z \Big|_{z=0} = \underbrace{x\mathbf{e}_x + y\mathbf{e}_y}_{=\mathbf{r}_{\text{sc}}(\varphi)} + \underbrace{z\mathbf{e}_z}_{=0} = \underbrace{r\mathbf{e}_r(\varphi)}_{=\underline{\mathbf{r}}} = \underline{\mathbf{r}}$$

Field Quantities / Feldgrößen

$$\{\underline{\mathbf{E}}(\underline{\mathbf{R}}, \omega), \underline{\mathbf{H}}(\underline{\mathbf{R}}, \omega), \underline{\mathbf{K}}_e(\underline{\mathbf{R}}, \omega), \underline{\mathbf{K}}_m(\underline{\mathbf{R}}, \omega)\} \Big|_{z=0} \rightarrow \{\underline{\mathbf{E}}(\underline{\mathbf{r}}, \omega), \underline{\mathbf{H}}(\underline{\mathbf{r}}, \omega), \underline{\mathbf{K}}_e(\underline{\mathbf{r}}, \omega), \underline{\mathbf{K}}_m(\underline{\mathbf{r}}, \omega)\}$$

$$\frac{\partial}{\partial z} \equiv 0$$

All Field Quantities and the Geometry are Independent of z /
Alle Feldgrößen und die Geometrie sind von z unabhängig



2-D Versions of EFIE and MFIE: TM and TE Case / 2D-Versionen von EFIE und MFIE: TM- und TE-Fall

Boundary Condition /
Randbedingung

$$\begin{aligned} \underline{\mathbf{n}}_{\text{sc}} \times \underline{\mathbf{E}}(\mathbf{r}, \omega) &= \underline{\mathbf{0}} & \Rightarrow & & \underline{\mathbf{n}}_{\text{sc}} \times \underline{\mathbf{H}}(\mathbf{r}, \omega) &= \underline{\mathbf{K}}_e(\mathbf{r}, \omega) \\ \rightarrow \underline{\mathbf{K}}_m(\mathbf{r}, \omega) &= \underline{\mathbf{0}} & & & \rightarrow \underline{\mathbf{K}}_e(\mathbf{r}, \omega) &\neq \underline{\mathbf{0}} \end{aligned}$$

$$\underbrace{\underline{\mathbf{n}}_{\text{sc}} \times \underline{\mathbf{E}}(\mathbf{r}, \omega)}_{=0} = \underline{\mathbf{n}}_{\text{sc}} \times \underline{\mathbf{E}}^{\text{in}}(\mathbf{r}, \omega) + \underline{\mathbf{n}}_{\text{sc}} \times \underline{\mathbf{E}}^{\text{sc}}(\mathbf{r}, \omega)$$

$$\begin{aligned} \underline{\mathbf{n}}_{\text{sc}} \times \underline{\mathbf{E}}^{\text{sc}}(\mathbf{r}, \omega) &= -\underline{\mathbf{n}}_{\text{sc}} \times \underline{\mathbf{E}}^{\text{in}}(\mathbf{r}, \omega) & \text{This means that the tangential component of the incident and scattered} \\ \underline{\mathbf{E}}_t^{\text{sc}}(\mathbf{r}, \omega) &= -\underline{\mathbf{E}}_t^{\text{in}}(\mathbf{r}, \omega) & \text{wavefield are pointing in the opposite direction at the scatterer surface /} \\ & & \text{Dies bedeutet, dass die Tangentialkomponente des einfallenden und gestreuten} \\ & & \text{Wellenfeldes auf der Streueroberfläche in die entgegengesetzte Richtung zeigen.} \end{aligned}$$

For the Derivation of the 2-D PEC TM EFIE we start from the 3-D Franz-Larmor version of EFIE for the Scattered Electric Field Strength for /
Zur Ableitung der 2D-PEC-TM-EFIE starten wir mit der 3D-Franz-Larmor-Version von EFIE für die gestreute elektrische Feldstärke für

$$\underline{\mathbf{R}} \in \mathbb{R}^3 \setminus \bar{V}_{\text{sc}}$$

Franz-Larmor version / Franz-Larmor-Version:

$$-\frac{1}{j\omega\epsilon_0} \underline{\mathbf{n}}_{\text{sc}} \times \nabla \times \nabla \times \underbrace{\iint_{\underline{\mathbf{R}}' \in S_{\text{sc}} = \partial V_{\text{sc}}} \underline{\mathbf{K}}_e(\underline{\mathbf{R}}', \omega) G(\underline{\mathbf{R}} - \underline{\mathbf{R}}', \omega) d^2 \underline{\mathbf{R}}'}_{= \underline{\mathbf{E}}^{\text{sc}}(\underline{\mathbf{R}}, \omega)} = -\underline{\mathbf{n}}_{\text{sc}} \times \underline{\mathbf{E}}^{\text{in}}(\underline{\mathbf{R}}, \omega)$$

2-D Versions of EFIE: TM Case / 2D-Versionen von EFIE: TM-Fall

Scattered Electric Field Strength /
Gestreeute elektrische Feldstärke

$$\underline{\mathbf{n}}_{\text{sc}} \times \left[-\frac{1}{j\omega\epsilon_0} \nabla \times \nabla \times \underbrace{\iint_{\underline{\mathbf{R}}' \in S_{\text{sc}} = \partial V_{\text{sc}}} \underline{\mathbf{K}}_e(\underline{\mathbf{R}}', \omega) G(\underline{\mathbf{R}} - \underline{\mathbf{R}}', \omega) d^2 \underline{\mathbf{R}}'}_{= \underline{\mathbf{E}}^{\text{sc}}(\underline{\mathbf{R}}, \omega)} \right] = -\underline{\mathbf{n}}_{\text{sc}} \times \underline{\mathbf{E}}^{\text{in}}(\underline{\mathbf{R}}, \omega)$$

$$\underline{\mathbf{E}}^{\text{sc}}(\underline{\mathbf{R}}, \omega) = -\frac{1}{j\omega\epsilon_0} \nabla \times \nabla \times \iint_{\underline{\mathbf{R}}' \in S_{\text{sc}} = \partial V_{\text{sc}}} \underline{\mathbf{K}}_e(\underline{\mathbf{R}}', \omega) G(\underline{\mathbf{R}} - \underline{\mathbf{R}}', \omega) d^2 \underline{\mathbf{R}}'$$

In the 2-D TM is only the E_z Component Unequal of Zero. That's Because we project
the Electric Field Strength Onto the Unit Vector in z Direction /

Im 2D-TM-Fall ist nur die E_z -Komponente ungleich von Null. Deshalb projizieren wir
den elektrische Feldstärkevektor auf den Einheitsvektor in z -Richtung

$$\underline{\mathbf{e}}_z \cdot \underline{\mathbf{E}}^{\text{sc}}(\underline{\mathbf{R}}, \omega) = E_z^{\text{sc}}(\underline{\mathbf{R}}, \omega)$$

We take only the z Component of the above Integral Equation for the observation point outside the scattering volume /
Wir nehmen nur die z -Komponente der oberen Integralgleichung für einen Beobachtungspunkt außerhalb des Streuvolumens

$$\underline{\mathbf{e}}_z \cdot \underline{\mathbf{E}}^{\text{sc}}(\underline{\mathbf{R}}, \omega) = -\frac{1}{j\omega\epsilon_0} \underline{\mathbf{e}}_z \cdot \nabla \times \nabla \times \iint_{\underline{\mathbf{R}}' \in S_{\text{sc}} = \partial V_{\text{sc}}} \underline{\mathbf{K}}_e(\underline{\mathbf{R}}', \omega) G(\underline{\mathbf{R}} - \underline{\mathbf{R}}', \omega) d^2 \underline{\mathbf{R}}'$$

2-D Versions of EFIE: TM Case / 2D-Versionen von EFIE: TM-Fall

Now we Apply the double curl operator and specialize the result for the 2-D TM case at the plane $z=0$. /
Nun wenden wir den doppelten Rotationsoperator an und spezialisieren das Ergebnis für die Ebene $z=0$.

$$\underline{e}_z \cdot \nabla \times \nabla \times \iint_{\mathbf{R}' \in S_{sc} = \partial V_{sc}} \underline{K}_c(\mathbf{R}', \omega) G(\mathbf{R} - \mathbf{R}', \omega) d^2 \mathbf{R}' = \underline{e}_z \cdot \iint_{\mathbf{R}' \in S_{sc} = \partial V_{sc}} \nabla \times \nabla \times \left[\underline{K}_c(\mathbf{R}', \omega) G(\mathbf{R} - \mathbf{R}', \omega) \right] d^2 \mathbf{R}'$$

We compute for the double curl operator /
Wir berechnen für den doppelten Rotationsoperator

$$\begin{aligned} \nabla \times \nabla \times \left[\underline{K}_c(\mathbf{R}', \omega) G(\mathbf{R} - \mathbf{R}', \omega) \right] &= \nabla \nabla \cdot \left[\underline{K}_c(\mathbf{R}', \omega) G(\mathbf{R} - \mathbf{R}', \omega) \right] - \nabla \cdot \nabla \left[\underline{K}_c(\mathbf{R}', \omega) G(\mathbf{R} - \mathbf{R}', \omega) \right] \\ &= \underline{K}_c(\mathbf{R}', \omega) \cdot \nabla \nabla G(\mathbf{R} - \mathbf{R}', \omega) - \underline{K}_c(\mathbf{R}', \omega) \nabla \cdot \nabla G(\mathbf{R} - \mathbf{R}', \omega) \end{aligned}$$

For all points outside the Scattering Volume we find /
Für alle Punkte außerhalb des Streuvolumens find wir

$$\begin{aligned} \nabla \nabla G(\mathbf{R} - \mathbf{R}', \omega) &= k_0^2 \left\{ - \left(\widehat{\mathbf{R} - \mathbf{R}'} \right) \left(\widehat{\mathbf{R} - \mathbf{R}'} \right) + \frac{j}{k_0 |\mathbf{R} - \mathbf{R}'|} \left[\underline{I} - 3 \left(\widehat{\mathbf{R} - \mathbf{R}'} \right) \left(\widehat{\mathbf{R} - \mathbf{R}'} \right) \right] \right. \\ &\quad \left. - \frac{1}{k_0^2 |\mathbf{R} - \mathbf{R}'|} \left[\underline{I} - 3 \left(\widehat{\mathbf{R} - \mathbf{R}'} \right) \left(\widehat{\mathbf{R} - \mathbf{R}'} \right) \right] \right\} G(\mathbf{R} - \mathbf{R}', \omega) \end{aligned}$$

$$\nabla \cdot \nabla G(\mathbf{R} - \mathbf{R}', \omega) = -k_0^2 G(\mathbf{R} - \mathbf{R}', \omega)$$

2-D Versions of EFIE: TM Case / 2D-Versionen von EFIE: TM-Fall

$$\nabla \times \nabla \times \left[\underline{K}_c(\mathbf{R}', \omega) G(\mathbf{R} - \mathbf{R}', \omega) \right] = \underline{K}_c(\mathbf{R}', \omega) \cdot \nabla \nabla G(\mathbf{R} - \mathbf{R}', \omega) - \underline{K}_c(\mathbf{R}', \omega) \nabla \cdot \nabla G(\mathbf{R} - \mathbf{R}', \omega)$$

We now consider the z independent case and an electric surface current density of the form /
Wir betrachten nun den von z unabhängigen Fall und eine elektrische Flächenstromdichte von der Form

$$\begin{aligned} \underline{K}_c(\mathbf{R}', \omega) &= \underline{K}_{e_z}^{\text{TM}}(\mathbf{R}', \omega) \\ &= K_{e_z}^{\text{TM}}(\mathbf{R}', \omega) \underline{e}_z \end{aligned}$$

and find /
und finden

$$\begin{aligned} \underline{e}_z \cdot \left[\underline{K}_c(\mathbf{R}', \omega) \cdot \nabla \nabla G(\mathbf{R} - \mathbf{R}', \omega) \right]_{z=0} &= \underline{e}_z \cdot \left[K_{e_z}^{\text{TM}}(\mathbf{R}', \omega) \underline{e}_z \cdot \nabla \nabla G(\mathbf{R} - \mathbf{R}', \omega) \right]_{z=0} \\ &= K_{e_z}^{\text{TM}}(\mathbf{R}', \omega) \underline{e}_z \cdot \underline{e}_z \cdot \nabla \nabla G(\mathbf{R} - \mathbf{R}', \omega) \Big|_{z=0} \\ &= \underbrace{K_{e_z}^{\text{TM}}(\mathbf{R}', \omega)}_{= \frac{\partial^2}{\partial z^2}} \cdot \nabla \nabla G(\mathbf{R} - \mathbf{R}', \omega) \Big|_{z=0} \\ &= K_{e_z}^{\text{TM}}(\mathbf{R}', \omega) \frac{\partial^2}{\partial z^2} G(\mathbf{R} - \mathbf{R}', \omega) \Big|_{z=0} \\ &= 0 \end{aligned}$$

2-D Versions of EFIE: TM Case / 2D-Versionen von EFIE: TM-Fall

$$\begin{aligned}
 \mathbf{e}_z \cdot \left[\mathbf{K}_c(\mathbf{R}', \omega) \nabla \cdot \nabla G(\mathbf{R} - \mathbf{R}', \omega) \right] \Big|_{z=0} &= \mathbf{e}_z \cdot \left[K_{ez}^{\text{TM}}(\mathbf{R}', \omega) \mathbf{e}_z \nabla \cdot \nabla G(\mathbf{R} - \mathbf{R}', \omega) \right] \Big|_{z=0} \\
 &= \left[K_{ez}^{\text{TM}}(\mathbf{R}', \omega) \underbrace{\mathbf{e}_z \cdot \nabla \cdot \nabla G(\mathbf{R} - \mathbf{R}', \omega)}_{=1} \right] \Big|_{z=0} \\
 &= \left[K_{ez}^{\text{TM}}(\mathbf{R}', \omega) \nabla \cdot \nabla G(\mathbf{R} - \mathbf{R}', \omega) \right] \Big|_{z=0} \\
 &\quad - k_0^2 G(\mathbf{R} - \mathbf{R}', \omega) \\
 &= -K_{ez}^{\text{TM}}(\mathbf{R}', \omega) k_0^2 G(\mathbf{R} - \mathbf{R}', \omega) \Big|_{z=0}
 \end{aligned}$$

$$\begin{aligned}
 \nabla \times \nabla \times \left[\mathbf{K}_c(\mathbf{R}', \omega) G(\mathbf{R} - \mathbf{R}', \omega) \right] \Big|_{z=0} &= \underbrace{\mathbf{K}_c(\mathbf{R}', \omega) \cdot \nabla \nabla G(\mathbf{R} - \mathbf{R}', \omega)}_{=0} - \underbrace{\mathbf{K}_c(\mathbf{R}', \omega) \nabla \cdot \nabla G(\mathbf{R} - \mathbf{R}', \omega)}_{=-K_{ez}^{\text{TM}}(\mathbf{R}', \omega) k_0^2 G(\mathbf{R} - \mathbf{R}', \omega)} \Big|_{z=0} \\
 &= K_{ez}^{\text{TM}}(\mathbf{R}', \omega) k_0^2 G(\mathbf{R} - \mathbf{R}', \omega) \Big|_{z=0}
 \end{aligned}$$

2-D Versions of EFIE: TM Case / 2D-Versionen von EFIE: TM-Fall

$$\begin{aligned}
 \mathbf{e}_z \cdot \nabla \times \nabla \times \iint_{\mathbf{R}' \in S_{\text{sc}} = \partial V_{\text{sc}}} \mathbf{K}_c(\mathbf{R}', \omega) G(\mathbf{R} - \mathbf{R}', \omega) d^2 \mathbf{R}' &= \mathbf{e}_z \cdot \iint_{\mathbf{R}' \in S_{\text{sc}} = \partial V_{\text{sc}}} \nabla \times \nabla \times \left[\mathbf{K}_c(\mathbf{R}', \omega) G(\mathbf{R} - \mathbf{R}', \omega) \right] d^2 \mathbf{R}' \\
 &= -j\omega \varepsilon_0 \mathbf{e}_z \cdot \mathbf{E}^{\text{sc}}(\mathbf{R}, \omega)
 \end{aligned}$$

$$\begin{aligned}
 \nabla \times \nabla \times \left[\mathbf{K}_c(\mathbf{R}', \omega) G(\mathbf{R} - \mathbf{R}', \omega) \right] \Big|_{z=0} &= \underbrace{\mathbf{K}_c(\mathbf{R}', \omega) \cdot \nabla \nabla G(\mathbf{R} - \mathbf{R}', \omega)}_{=0} - \underbrace{\mathbf{K}_c(\mathbf{R}', \omega) \nabla \cdot \nabla G(\mathbf{R} - \mathbf{R}', \omega)}_{=-K_{ez}^{\text{TM}}(\mathbf{R}', \omega) k_0^2 G(\mathbf{R} - \mathbf{R}', \omega)} \Big|_{z=0} \\
 &= K_{ez}^{\text{TM}}(\mathbf{R}', \omega) k_0^2 G(\mathbf{R} - \mathbf{R}', \omega) \Big|_{z=0}
 \end{aligned}$$

$$\begin{aligned}
 \mathbf{e}_z \cdot \iint_{\mathbf{R}' \in S_{\text{sc}} = \partial V_{\text{sc}}} \nabla \times \nabla \times \left[\mathbf{K}_c(\mathbf{R}', \omega) G(\mathbf{R} - \mathbf{R}', \omega) \right] d^2 \mathbf{R}' \Big|_{z=0} &= \iint_{\mathbf{R}' \in S_{\text{sc}} = \partial V_{\text{sc}}} K_{ez}^{\text{TM}}(\mathbf{R}', \omega) k_0^2 G(\mathbf{R} - \mathbf{R}', \omega) d^2 \mathbf{R}' \Big|_{z=0} \\
 &= -j\omega \varepsilon_0 \mathbf{e}_z \cdot \mathbf{E}^{\text{sc}}(\mathbf{R}, \omega) \Big|_{z=0}
 \end{aligned}$$

$$\begin{aligned}
 \mathbf{e}_z \cdot \mathbf{E}^{\text{sc}}(\mathbf{R}, \omega) \Big|_{z=0} &= -\frac{k_0^2}{j\omega \varepsilon_0} \iint_{\mathbf{R}' \in S_{\text{sc}} = \partial V_{\text{sc}}} K_{ez}^{\text{TM}}(\mathbf{R}', \omega) G(\mathbf{R} - \mathbf{R}', \omega) d^2 \mathbf{R}' \Big|_{z=0} \\
 &= j\omega \mu_0 \iint_{\mathbf{R}' \in S_{\text{sc}} = \partial V_{\text{sc}}} K_{ez}^{\text{TM}}(\mathbf{R}', \omega) G(\mathbf{R} - \mathbf{R}', \omega) d^2 \mathbf{R}' \Big|_{z=0}
 \end{aligned}$$

$$\mathbf{E}_z^{\text{sc}}(\mathbf{R}, \omega) \Big|_{z=0} = j\omega \mu_0 \iint_{\mathbf{R}' \in S_{\text{sc}} = \partial V_{\text{sc}}} K_{ez}^{\text{TM}}(\mathbf{R}', \omega) G(\mathbf{R} - \mathbf{R}', \omega) d^2 \mathbf{R}' \Big|_{z=0}$$

2-D Versions of EFIE: TM Case / 2D-Versionen von EFIE: TM-Fall

$$\begin{aligned} E_z^{\text{sc}}(\mathbf{R}, \omega) \Big|_{z=0} &= j\omega\mu_0 \left[\oint\!\!\!\oint_{\mathbf{R}' \in S_{\text{sc}} = \partial V_{\text{sc}}} \mathbf{K}_{\text{e}z}^{\text{TM}}(\mathbf{R}', \omega) G(\mathbf{R} - \mathbf{R}', \omega) d^2 \mathbf{R}' \right] \Big|_{z=0} \\ &= j\omega\mu_0 \oint_{\mathbf{r}' \in C_{\text{sc}} = \partial S_{\text{sc}}} \mathbf{K}_{\text{e}z}^{\text{TM}}(\mathbf{r}', \omega) \left[\int_{z'=-\infty}^{\infty} G(\mathbf{R} - \mathbf{R}', \omega) dz' \right] \Big|_{z=0} d\mathbf{r}' \end{aligned}$$

$$E_z^{\text{sc}}(\mathbf{r}, \omega) = j\omega\mu_0 \oint_{\mathbf{r}' \in C_{\text{sc}} = \partial S_{\text{sc}}} \mathbf{K}_{\text{e}z}^{\text{TM}}(\mathbf{r}', \omega) \left[\int_{z'=-\infty}^{\infty} G(\mathbf{R} - \mathbf{R}', \omega) dz' \right] \Big|_{z=0} d\mathbf{r}'$$

$$\begin{aligned} \left[\int_{z'=-\infty}^{\infty} G(\mathbf{R} - \mathbf{R}', \omega) dz' \right] \Big|_{z=0} &= \left[\int_{z'=-\infty}^{\infty} \frac{e^{jk_0 |\mathbf{R} - \mathbf{R}'|}}{4\pi |\mathbf{R} - \mathbf{R}'|} dz' \right] \Big|_{z=0} \\ &= \int_{z'=-\infty}^{\infty} \frac{e^{jk_0 |\mathbf{r} - \mathbf{r}'|}}{4\pi |\mathbf{r} - \mathbf{r}'|} dz' \\ &= \frac{j}{4} H_0^{(1)}(k_0 |\mathbf{r} - \mathbf{r}'|) \quad H_0^{(1)}(\cdot) \quad \text{Hankel function of 1st kind and 0th order /} \\ & \quad \text{Hankel-Funktion der 1. Art und 0. Ordnung} \end{aligned}$$

Scalar 2-D Green's function of free-space /
Skalare 2-D Greensche Funktion des Freiraumes

$$G(\mathbf{r} - \mathbf{r}', \omega) = \frac{j}{4} H_0^{(1)}(k_0 |\mathbf{r} - \mathbf{r}'|)$$

2-D Versions of EFIE: TM Case / 2D-Versionen von EFIE: TM-Fall

$$E_z^{\text{sc}}(\mathbf{r}, \omega) = j\omega\mu_0 \oint_{\mathbf{r}' \in C_{\text{sc}} = \partial S_{\text{sc}}} \mathbf{K}_{\text{e}z}^{\text{TM}}(\mathbf{r}', \omega) G(\mathbf{r} - \mathbf{r}', \omega) d\mathbf{r}', \quad \mathbf{r} \in C_{\text{sc}}$$

Scalar 2-D Green's function of free-space /
Skalare 2-D Greensche Funktion des Freiraumes

$$G(\mathbf{r} - \mathbf{r}', \omega) = \frac{j}{4} H_0^{(1)}(k_0 |\mathbf{r} - \mathbf{r}'|)$$

Integral representation of the scattered field at the scatterer /
Integraldarstellung des Streufeldes auf dem Streuer

$$E_z^{\text{sc}}(\mathbf{r}, \omega) = j\omega\mu_0 \oint_{\mathbf{r}' \in C_{\text{sc}} = \partial S_{\text{sc}}} \mathbf{K}_{\text{e}z}^{\text{TM}}(\mathbf{r}', \omega) G(\mathbf{r} - \mathbf{r}', \omega) d\mathbf{r}', \quad \mathbf{r} \in C_{\text{sc}}$$

2-D PEC TM EFIE for the z component of the electric field strength /
2D-IEL-TM-EFIE für die z-Komponente der elektrischen Feldstärke

$$E_z^{\text{sc}}(\mathbf{r}, \omega) = -E_z^{\text{in}}(\mathbf{r}, \omega), \quad \mathbf{r} \in C_{\text{sc}}$$

Finally we obtain for the 2-D PEC TM EFIE / Schließlich erhalten wir für die 2D-IEL-TM-EFIE

$$j\omega\mu_0 \oint_{\mathbf{r}' \in C_{\text{sc}} = \partial S_{\text{sc}}} \mathbf{K}_{\text{e}z}^{\text{TM}}(\mathbf{r}', \omega) G(\mathbf{r} - \mathbf{r}', \omega) d\mathbf{r}' = -E_z^{\text{in}}(\mathbf{r}, \omega), \quad \mathbf{r} \in C_{\text{sc}}$$

This is a *Fredholm integral equation of the 1. kind* in form of a *closed line integral* for the *unknown* electric surface current density for a *known* incident field. /
Dies ist eine *Fredholmsche Integralgleichung 1. Art* in Form eines *geschlossenen Linienintegrals* für die *unbekannte* elektrische Flächenladungsdichte für ein *bekanntes* einfallendes Feld.

Method of Moments (MoM) – Introduction / Momenten-Methode (MoM) – Einleitung

$$\begin{array}{l} \text{2-D-PEC-TM-EFIE /} \\ \text{2D-IEL-TM-EFIE} \end{array} \quad j\omega\mu_0 \oint_{\mathbf{r}' \in C_{sc} = \partial\Delta_{sc}} \mathbf{K}_{ez}^{\text{TM}}(\mathbf{r}', \omega) G(\mathbf{r} - \mathbf{r}', \omega) d\mathbf{r}' = -E_z^{\text{in}}(\mathbf{r}, \omega), \quad \mathbf{r} \in C_{sc}$$



Linear Operator Equation /
Lineare Operatorgleichung

$$\mathcal{L}\{f\} = g$$



Linear Operator Equation /
Lineare Operatorgleichung

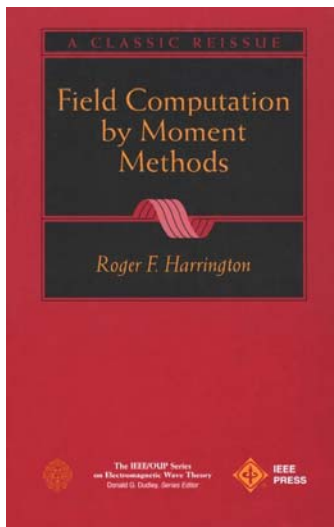
$$[\mathbf{L}]\{\mathbf{f}\} = \{\mathbf{g}\}$$

Method of Moments (MoM) /
Momentenmethode

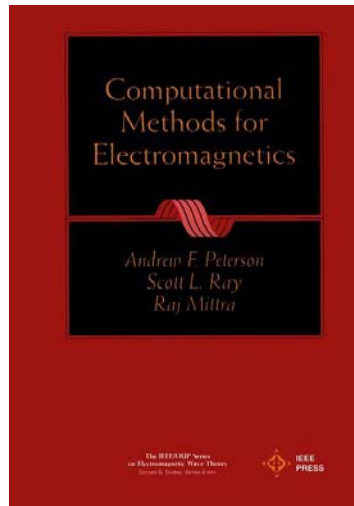
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Method of Moments (MoM) – Introduction / Momenten-Methode (MoM) – Einleitung



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Method of Moments (MoM) – Linear Operator Equation / Momenten-Methode (MoM) – Lineare Operatorgleichung

Linear Operator Equation /
Lineare Operatorgleichung

$$\mathcal{L}\{f\} = g$$

$[\mathbf{A}]\{\mathbf{x}\} = \{\mathbf{b}\}$ (Linear) Matrix Equation /
(Lineare) Matrixgleichung

with the Properties / mit den Eigenschaften

- $\mathbb{D}\{\mathcal{L}\}$ is the **Domain** of \mathcal{L} . /
 $\mathbb{D}\{\mathcal{L}\}$ ist der **Definitionsbereich** von \mathcal{L} .
- $\mathbb{R}\{\mathcal{L}\}$ is the **Range** or Co-domain of \mathcal{L} . /
 $\mathbb{R}\{\mathcal{L}\}$ ist der **Wertebereich** von \mathcal{L} .
- \mathbb{D} and \mathbb{R} are **Function Spaces** and $f \in \mathbb{D}, g \in \mathbb{R}$. /
 \mathbb{D} und \mathbb{R} sind **Funktionsräume** und $f \in \mathbb{D}, g \in \mathbb{R}$.
- The Functional or **Inner Product** is defined by /
Das Funktional oder **inneres Produkt** ist definiert durch

$$\langle f_1, f_2 \rangle := \int_{\mathbb{D}} f_1 f_2^* d\mathbb{D}$$

***: Conjugate Complex /
***: konjugiert komplex

Method of Moments (MoM) – Basis Function Expansion / Momenten-Methode (MoM) – Basisfunktionsentwicklung

Linear Operator Equation /
Lineare Operatorgleichung

$$\mathcal{L}\{f\} = g$$

Basis Function Expansion / Basisfunktionsentwicklung

Let α_n a Basis in \mathbb{D} , i.e. the α_n spans the domain \mathbb{D} , then we can represent f in form of series /
Sei α_n eine Basis von \mathbb{D} , d.h. die α_n spannen den Raum \mathbb{D} auf, dann lässt sich f in Form einer Reihe darstellen

$$f = \sum_n c_n \alpha_n$$

Function /
Funktion

Coefficients /
Koeffizienten

Basis Functions /
Basisfunktionen

Because of the Linearity of the Operator \mathcal{L} / Wegen der Linearität des Operator \mathcal{L}

$$\begin{aligned} \mathcal{L}\{f\} &= \mathcal{L}\left\{\sum_n c_n \alpha_n\right\} \\ &= \sum_n c_n \mathcal{L}\{\alpha_n\} \\ &= g \end{aligned}$$

Method of Moments (MoM) – Formulation (2) / Momenten-Methode (MoM) – Formulierung (2)

Linear Operator Equation /
Lineare Operatorgleichung

$$\mathcal{L}\{f\} = g$$

Testing Procedure: Weighting Functions / Testprozedur: Gewichtungsfunktionen

Let w_m a the weighting functions – Testing Functions – of \mathbb{R} , then the following projection theorem holds /
Seien w_m die Gewichtungsfunktionen – Testfunktionen – in \mathbb{R} , dann gilt der Projektionssatz

$$\langle w_m, \mathcal{L}\{f\} \rangle = \langle w_m, g \rangle$$

$$\langle w_m, \mathcal{L}\{f\} - g \rangle = 0 \quad \forall m$$

$$\langle w_m, \mathcal{L}\{\sum_n c_n \alpha_n\} \rangle = \langle w_m, g \rangle$$

$$\sum_n c_n \langle w_m, \mathcal{L}\{\alpha_n\} \rangle = \langle w_m, g \rangle$$

System of Linear Equations / Linear Gleichungssystem

$$[\mathbf{L}]\{\mathbf{f}\} = \{\mathbf{g}\} \quad \leftrightarrow \quad \sum_n L_{mn} f_n = g_m$$

Method of Moments (MoM) – Selection of Basis and Weighting (Testing) Functions / Momenten-Methode (MoM) – Wahl der Basis- und Gewichtungs(Test)funktionen

Basis Functions are α_n and Weighting Functions (Testing Functions) are w_m /
Basisfunktionen sind die α_n und Gewichtungsfunktionen (Testfunktionen) sind die w_m

1. Let $w_m = \alpha_n$, then we call this the Method of Galerkin /
Sind die $w_m = \alpha_n$, dann sprechen wir von der Galerkin-Methode
2. Let $w_m = \mathcal{L}\{\alpha_m\}$, which results in the Least Square Method. The Method of Moments gives then an approximation with the least quadratic mean value. /
Sind die $w_m = \mathcal{L}\{\alpha_m\}$, dann erhält man die Methode der kleinsten Fehlerquadrate. Die Momentan-Methode liefert dann eine Approximation mit dem kleinsten quadratischen Mittelwert.

$$L_{mn} = \langle \mathcal{L}\{\alpha_m\}, \mathcal{L}\{\alpha_n\} \rangle$$

Now we define a error functional / Nun definieren wir ein Fehlerfunktional

$$r^N := \sum_{n=1}^N c_n \alpha_n - g$$

and build the mean quadratic error / und bilden den mittleren quadratischen Fehler

$$\langle r^N, r^N \rangle$$

then we minimize the error if / so wird der Fehler minimal für

$$w_m = \mathcal{L}\{\alpha_m\}$$

Method of Moments (MoM) – Selection of Basis and Weighting (Testing) Functions / Momenten-Methode (MoM) – Wahl der Basis- und Gewichtungs(Test)funktionen

Basis Functions are α_n and Weighting Functions (Testing Functions) are w_m /
Basisfunktionen sind die α_n und Gewichtungsfunktionen (Testfunktionen) sind die w_m

1. Entire Domain Basis Functions / Ganzbereichsbasisfunktionen

The basis functions α_n are defined over the complete domain \mathbb{D} .

Examples are:

$$\sin(x), \cos(x), e^{jx}$$

Die Basisfunktionen α_n sind über den gesamten Definitionsbereich \mathbb{D} definiert.

Beispiele sind:

$$\sin(x), \cos(x), e^{jx}$$

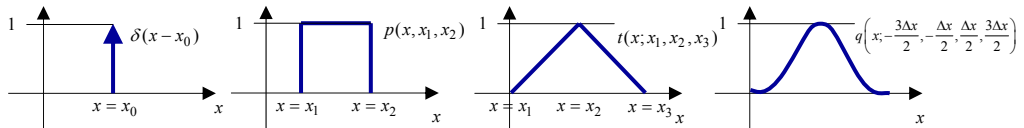
2. Subdomain Basis Functions / Unterbereichsbasisfunktionen

The basis functions α_n are defined over subdomain of the domain \mathbb{D} .

Examples are: Delta Function, Rectangular Pulse (or Piecewise-Constant) Function, Triangular Pulse Function, Quadratic Spline Function

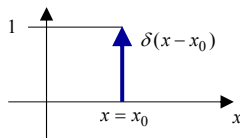
Die Basisfunktionen α_n sind über einen Unterbereich des Bereichs \mathbb{D} definiert.

Beispiele sind: Delta-Funktion, Rechteckimpuls-Funktion, Dreieckimpuls-Funktion, Quadratische Spline Funktion



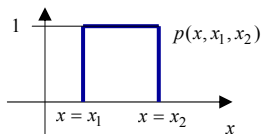
Method of Moments (MoM) – Selection of Basis and Weighting (Testing) Functions / Momenten-Methode (MoM) – Wahl der Basis- und Gewichtungs(Test)funktionen

Delta Function / Delta-Funktion



$$B_0(x) = \delta(x - x_0)$$

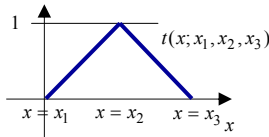
Rectangular Pulse (or Piecewise-Constant) Function / Rechteckimpuls-Funktion (oder stückweise konstante Funktion)



$$B_1(x) = p(x; x_1, x_2) = \begin{cases} 1 & x_1 \leq x \leq x_2 \\ 0 & \text{otherwise / sonst} \end{cases}$$

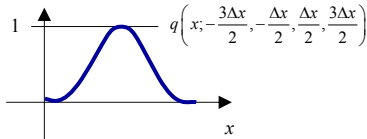
Method of Moments (MoM) – Selection of Basis and Weighting (Testing) Functions / Momenten-Methode (MoM) – Wahl der Basis- und Gewichtungs(Test)funktionen

Triangular Pulse Function / Dreieckimpulsfunktion



$$B_2(x) = t(x; x_1, x_2, x_3) = \begin{cases} \frac{x-x_1}{x_2-x_1} & x_1 \leq x \leq x_2 \\ \frac{x_3-x}{x_3-x_2} & x_2 < x \leq x_3 \\ \text{sonst} & \text{sonst} \\ 0 & \text{otherwise / sonst} \end{cases}$$

Quadratic Spline Function / Quadratische Spline-Funktion



$$B_2(x) = q\left(x; -\frac{3\Delta x}{2}, -\frac{\Delta x}{2}, \frac{\Delta x}{2}, \frac{3\Delta x}{2}\right) = \begin{cases} 0 & x < -\frac{3\Delta x}{2} \\ \frac{9}{8} + \frac{3x}{2\Delta x} + \frac{x^2}{2(\Delta x)^2} & -\frac{3\Delta x}{2} \leq x < -\frac{\Delta x}{2} \\ \frac{3}{4} - \frac{x^2}{(\Delta x)^2} & -\frac{\Delta x}{2} \leq x < \frac{\Delta x}{2} \\ \frac{9}{8} - \frac{3x}{2\Delta x} + \frac{x^2}{2(\Delta x)^2} & \frac{\Delta x}{2} \leq x < \frac{3\Delta x}{2} \\ 0 & x > \frac{3\Delta x}{2} \end{cases}$$

Method of Moments (MoM) – Example: Solution of a 1-D Boundary Value Problem / Momenten-Methode (MoM) – Beispiel: Lösung eines 1D-Randwertproblems

Given is the boundary value problem / Gegeben ist der Randwertproblem

$$-\frac{d^2}{dx^2} f(x) = 1 + 4x^2$$

$f(x)$ continuous for $x = [0, 1]$
Boundary conditions: $f(0) = f(1) = 0$ /
 $f(x)$ stetig für $x = [0, 1]$
Randbedingungen: $f(0) = f(1) = 0$

Determine /
Bestimme $f(x) = ?$

Basis Function Expansion /
Basisfunktionsentwicklung

$$f(x) = \sum_{n=1}^N c_n \alpha_n(x)$$

Basis Functions /
Basisfunktionen

$$\alpha_n(x) = x - x^{n+1}$$

Ensures the Boundary conditions /
Erfüllt die Randbedingungen

$$\alpha_n(0) = \alpha_n(1) = 0$$

Inner Product /
Inneres Produkt $\langle f(x), g(x) \rangle := \int_{x=0}^1 f(x)g(x)dx$

$$\langle f_1, f_2 \rangle := \int_{\mathbb{D}} f_1 f_2^* d\mathbb{D}$$

$\mathbb{D} \rightarrow x = [0, 1]$

**Method of Moments (MoM) – Example: Solution of a 1-D Boundary Value Problem /
Momenten-Methode (MoM) – Beispiel: Lösung eines 1D-Randwertproblems**

$$w_m(x) = \mathcal{L}\{\alpha_m(x)\}$$

$$\mathcal{L} = -\frac{d^2}{dx^2}$$

Testing Functions /
Testfunktionen

$$w_m(x) = \mathcal{L}\{x - x^{m+1}\}$$

$$= -\frac{d^2}{dx^2}(x - x^{m+1})$$

$$= m(m+1)x^{m-1}$$

$$\mathcal{L}\{f\} = g$$

$$\langle w_m(x), \mathcal{L}\{f(x)\} \rangle = \langle w_m(x), g(x) \rangle$$

$$g(x) = 1 + 4x^2$$

**Method of Moments (MoM) – Example: Solution of a 1-D Boundary Value Problem /
Momenten-Methode (MoM) – Beispiel: Lösung eines 1D-Randwertproblems**

$$\langle w_m(x), \mathcal{L}\{f(x)\} \rangle = \langle w_m(x), g(x) \rangle$$

$$\langle w_m(x), \mathcal{L}\{f(x)\} \rangle = \left\langle m(m+1)x^{m-1}, -\frac{d}{dx} \sum_{n=1}^N c_n (x - x^{n-1}) \right\rangle$$

$$= \sum_{n=1}^N c_n \langle m(m+1)x^{m-1}, n(n+1)x^{n-1} \rangle$$

$$= m(m+1) \sum_{n=1}^N n(n+1) c_n \int_{x=0}^1 x^{m-1} x^{n-1} dx$$

$$= m(m+1) \sum_{n=1}^N \frac{n(n+1)}{m+n-1} c_n$$

$$\langle w_m(x), g(x) \rangle = \langle m(m+1)x^{m-1}, (1 + 4x^2) \rangle$$

$$= \int_{x=0}^1 m(m+1)x^{m-1} (1 + 4x^2) dx$$

$$= m(m+1) \int_{x=0}^1 (x^{m-1} + 4x^{m+1}) dx$$

$$= \frac{(5m+1)(m+1)}{m+2}$$

$$[\mathbf{L}]\{\mathbf{f}\} = \{\mathbf{g}\} \quad \sum_n L_{mn} f_n = g_m$$

$$L_{mn} = m(m+1) \frac{n(n+1)}{m+n-1}$$

$$f_n = c_n$$

$$g_m = \frac{(5m+1)(m+1)}{m+2}$$

**Method of Moments (MoM) – Example: Solution of a 1-D Boundary Value Problem /
Momenten-Methode (MoM) – Beispiel: Lösung eines 1D-Randwertproblems**

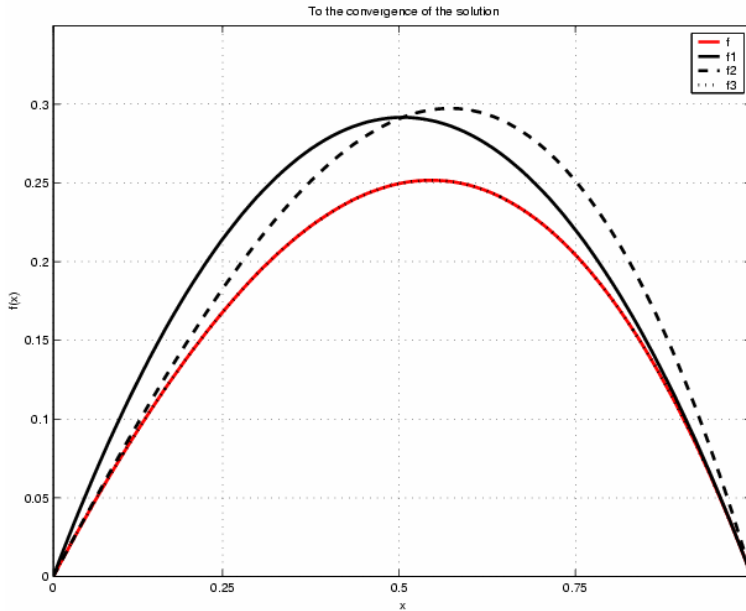
$$\begin{array}{lll}
 N = 1 & L_{11} = 4 & f_1(x) = \sum_{n=1}^1 c_n \alpha_n(x) \\
 & g_1 = \frac{14}{3} & = \sum_{n=1}^1 c_n (x - x^{n+1}) \\
 & f_1 = c_1 = \frac{7}{6} & = \frac{7}{6} (x - x^2) \\
 & & \mathcal{L}\{f_1(x)\} = \frac{7}{3} \\
 & & \neq 1 + 4x^2
 \end{array}$$

$$\begin{array}{lll}
 N = 2 & [\mathbf{L}] = \begin{bmatrix} 4 & 6 \\ 6 & 12 \end{bmatrix} & f_2(x) = \sum_{n=1}^2 c_n \alpha_n(x) \\
 & \{\mathbf{g}\} = \left\{ \begin{array}{l} 14 \\ 3 \\ 9 \end{array} \right\} & = \sum_{n=1}^2 c_n (x - x^{n+1}) \\
 & \{\mathbf{f}\}_2 = \{\mathbf{c}\}_2 = \left\{ \begin{array}{l} 1 \\ 6 \\ 2 \\ 3 \end{array} \right\} & = \frac{1}{6} (x - x^2) + \frac{2}{3} (x - x^3) \\
 & & = \frac{5}{6} x - \frac{1}{6} x^2 - \frac{2}{3} x^3 \\
 & & \mathcal{L}\{f_2(x)\} = \frac{1}{3} + 4x \\
 & & \neq 1 + 4x^2
 \end{array}$$

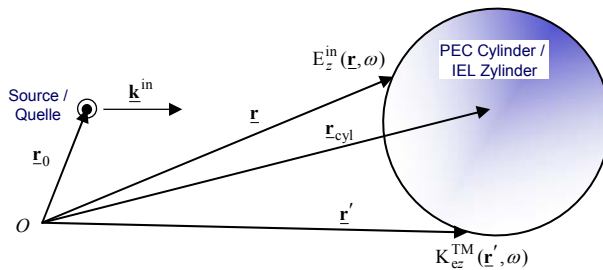
**Method of Moments (MoM) – Example: Solution of a 1-D Boundary Value Problem /
Momenten-Methode (MoM) – Beispiel: Lösung eines 1D-Randwertproblems**

$$\begin{array}{lll}
 N = 3 & [\mathbf{L}] = \begin{bmatrix} 4 & 6 & 8 \\ 6 & 12 & 18 \\ 8 & 18 & \frac{144}{5} \end{bmatrix} & f_3(x) = \sum_{n=1}^3 c_n \alpha_n(x) \\
 & \{\mathbf{g}\} = \left\{ \begin{array}{l} 14 \\ 3 \\ 9 \\ \frac{68}{5} \end{array} \right\} & = \sum_{n=1}^3 c_n (x - x^{n+1}) \\
 & \{\mathbf{f}\}_3 = \{\mathbf{c}\}_3 = \left\{ \begin{array}{l} 1 \\ 2 \\ 0 \\ 1 \\ 3 \end{array} \right\} & = \frac{1}{2} (x - x^2) + \frac{1}{3} (x - x^4) \\
 & & = \frac{5}{6} x - \frac{1}{2} x^2 - \frac{1}{3} x^4 \\
 & & \mathcal{L}\{f_3(x)\} = 1 + 4x^2
 \end{array}$$

Method of Moments (MoM) – Example: Solution of a 1-D Boundary Value Problem / Momenten-Methode (MoM) – Beispiel: Lösung eines 1D-Randwertproblems



EM Scattering by a Perfectly Electrically Conducting Cylinder: EFIE Discretized in the 2-D TM Case with Pulse Basis and Delta Testing Functions / EM-Streuung an einem ideal elektrisch leitendem Zylinder: EFIE diskretisiert im 2D-TM-Fall mit Impuls-Basisfunktionen und Delta-Testfunktionen



2-D Case /
2D-Fall

$$\mathbf{R} = \underbrace{r \mathbf{e}_r(\varphi)}_{=\mathbf{r}} + z \underbrace{\mathbf{e}_z(\varphi)}_{=\mathbf{0}}$$

$$= \mathbf{r}$$

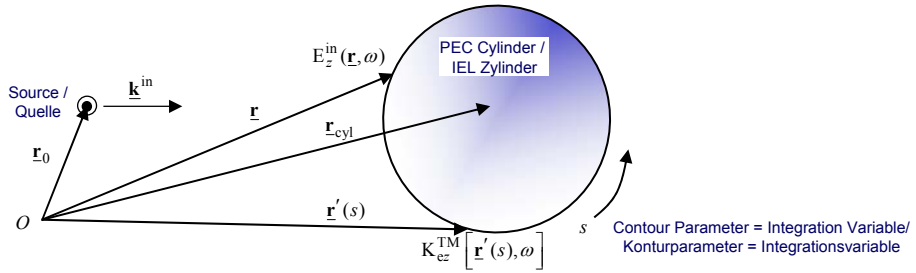
2-D PEC TM EFIE / 2D-IEL-TM-EFIE

$$j\omega\mu_0 \oint_{\mathbf{r}' \in C_{sc} = \partial S_{sc}} \mathbf{K}_{ez}^{TM}(\mathbf{r}', \omega) G(\mathbf{r} - \mathbf{r}', \omega) d\mathbf{r}' = -E_z^{in}(\mathbf{r}, \omega), \quad \mathbf{r} \in C_{sc}$$

This is a *Fredholm integral equation of the 1. kind* in form of a *closed line integral* for the *unknown* electric surface current density for a *known* incident field. /
Dies ist eine *Fredholmsche Integralgleichung 1. Art* in Form eines *geschlossenen Linienintegrals* für die *unbekannte* elektrische Flächenladungsdichte für ein *bekanntes* einfallendes Feld.

$$G(\mathbf{r} - \mathbf{r}', \omega) = \frac{j}{4} H_0^{(1)}(k_0 |\mathbf{r} - \mathbf{r}'|)$$

EM Scattering by a Perfectly Electrically Conducting Cylinder: EFIE Discretized in the 2-D TM Case with Pulse Basis and Delta Testing Functions / EM-Streuung an einem ideal elektrisch leitendem Zylinder: EFIE diskretisiert im 2D-TM-Fall mit Impuls-Basisfunktionen und Delta-Testfunktionen



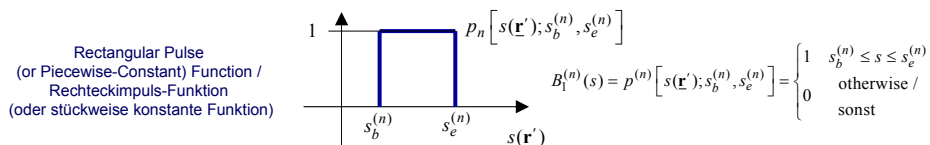
$$\begin{aligned} \underline{r}' &\rightarrow \underline{r}'(s) \\ \mathbf{K}_{ez}^{\text{TM}}(\underline{r}', \omega) &\rightarrow \mathbf{K}_{ez}^{\text{TM}}[\underline{r}'(s), \omega] \quad \underline{r}'(s) \in C_{sc} \quad C_{sc} : s_b \leq s \leq s_e \\ G(\underline{r} - \underline{r}') &\rightarrow G(\underline{r} - \underline{r}'(s), \omega) \end{aligned}$$

$$E_z^{\text{in}}(\underline{r}, \omega) = -j\omega\mu_0 \int_{s=s_b}^{s_e} G[\underline{r} - \underline{r}'(s), \omega] \mathbf{K}_{ez}^{\text{TM}}[\underline{r}'(s), \omega] d\underline{r}'(s) \quad \underline{r} \in C_{sc}$$

EM Scattering by a Perfectly Electrically Conducting Cylinder: EFIE Discretized in the 2-D TM Case with Rectangular Pulse Basis and Delta Testing Functions / EM-Streuung an einem ideal elektrisch leitendem Zylinder: EFIE diskretisiert im 2D-TM-Fall mit Rechteckimpuls-Basisfunktionen und Delta-Testfunktionen

$$E_z^{\text{in}}(\underline{r}, \omega) = -j\omega\mu_0 \int_{s=s_b}^{s_e} G[\underline{r} - \underline{r}'(s), \omega] \mathbf{K}_{ez}^{\text{TM}}[\underline{r}'(s), \omega] d\underline{r}'(s) \quad \underline{r} \in C_{sc}$$

**Basis Function Expansion using Rectangular Pulse Basis /
Basisfunktionsentwicklung mit Rechteckimpulsfunktionen**



$$\mathbf{K}_{ez}^{\text{TM}}[\underline{r}'(s), \omega] \approx \sum_{n=1}^N \mathbf{K}_{ez}^{\text{TM}(n)}(\omega) p^{(n)}[s(\underline{r}'); s_b^{(n)}, s_e^{(n)}]$$

$$\begin{aligned} E_z^{\text{in}}(\underline{r}, \omega) &\approx -j\omega\mu_0 \sum_{n=1}^N \mathbf{K}_{ez}^{\text{TM}(n)}(\omega) \int_{s=s_b}^{s_e} G[\underline{r} - \underline{r}'(s), \omega] p^{(n)}[s(\underline{r}'); s_b^{(n)}, s_e^{(n)}] d\underline{r}'(s) \quad \underline{r} \in C_{sc} \\ &\approx -j\omega\mu_0 \sum_{n=1}^N \mathbf{K}_{ez}^{\text{TM}(n)}(\omega) \int_{s=s_b^{(n)}}^{s_e^{(n)}} G[\underline{r} - \underline{r}'(s), \omega] d\underline{r}'(s) \end{aligned}$$

EM Scattering by a Perfectly Electrically Conducting Cylinder: EFIE Discretized in the 2-D TM Case with Pulse Basis and Delta Testing Functions / EM-Streuung an einem ideal elektrisch leitendem Zylinder: EFIE diskretisiert im 2D-TM-Fall mit Impuls-Basisfunktionen und Delta-Testfunktionen

$$E_z^{\text{in}}(\mathbf{r}, \omega) \approx -j\omega\mu_0 \sum_{n=1}^N K_{ez}^{\text{TM}(n)}(\omega) \int_{s=s_b^{(n)}}^{s_e^{(n)}} G[\mathbf{r}-\mathbf{r}'(s), \omega] d\mathbf{r}'(s)$$

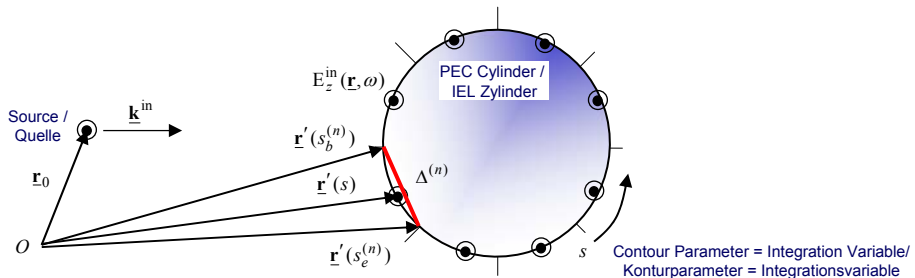
$$G[\mathbf{r}-\mathbf{r}'(s), \omega] = \frac{j}{4} H_0^{(1)}[k_0 |\mathbf{r}-\mathbf{r}'(s)|]$$

$$E_z^{\text{in}}(\mathbf{r}, \omega) \approx -j\omega\mu_0 \sum_{n=1}^N K_{ez}^{\text{TM}(n)}(\omega) \int_{s=s_b^{(n)}}^{s_e^{(n)}} \frac{j}{4} H_0^{(1)}[k_0 |\mathbf{r}-\mathbf{r}'(s)|] d\mathbf{r}'(s)$$

$$\approx \frac{\omega\mu_0}{4} \sum_{n=1}^N K_{ez}^{\text{TM}(n)}(\omega) \int_{s=s_b^{(n)}}^{s_e^{(n)}} H_0^{(1)}[k_0 |\mathbf{r}-\mathbf{r}'(s)|] d\mathbf{r}'(s)$$

$$\int_{s=s_b^{(n)}}^{s_e^{(n)}} H_0^{(1)}[k_0 |\mathbf{r}-\mathbf{r}'(s)|] d\mathbf{r}'(s) = ?$$

EM Scattering by a Perfectly Electrically Conducting Cylinder: EFIE Discretized in the 2-D TM Case with Pulse Basis and Delta Testing Functions / EM-Streuung an einem ideal elektrisch leitendem Zylinder: EFIE diskretisiert im 2D-TM-Fall mit Impuls-Basisfunktionen und Delta-Testfunktionen



$$\Delta^{(n)} = \left| \mathbf{r}'(s_b^{(n)}) - \mathbf{r}'(s_e^{(n)}) \right|$$

$$\int_{s=s_b^{(n)}}^{s_e^{(n)}} d\mathbf{r}'(s) \approx \left| \mathbf{r}'(s_b^{(n)}) - \mathbf{r}'(s_e^{(n)}) \right|$$

$$= \Delta^{(n)}$$

EM Scattering by a Perfectly Electrically Conducting Cylinder: EFIE Discretized in the 2-D TM Case with Pulse Basis and Delta Testing Functions / EM-Streuung an einem ideal elektrisch leitendem Zylinder: EFIE diskretisiert im 2D-TM-Fall mit Impuls-Basisfunktionen und Delta-Testfunktionen

**Power Series Approximation of the Main Diagonal Elements /
Potenzreihenapproximation der Hauptdiagonalelemente**

$$H_0^{(1)}(z) = J_0(z) + jN_0(z)?$$

**End of 3rd Lecture /
Ende der 3. Vorlesung**